



TITLE OF THE INVENTION

Hydrodynamic bearing and disk recording/reproducing apparatus

BACKGROUND OF THE INVENTION

The present invention relates to hydrodynamic bearings and
5 disk recording/reproducing apparatuses equipped with them.

Disk recording/reproducing apparatuses include magnetic
disks and magnetically or optically perform reading and writing
of data for the magnetic disks while revolving the magnetic disks.
Further increases in capacity and speedups of data transfers are
10 required of disk recording/reproducing apparatuses. Accordingly,
it is desired that revolutions of the magnetic disks become still
faster and are stabilized with still higher precision.
Hydrodynamic bearings are suitable for such high-speed and
high-precision rotary drive systems.

15 FIG. 6 is a cross-sectional view showing an example of
conventional hydrodynamic bearings. The top end of a shaft 31 is
fixed on the center of a hub 36. A flange 33 in an annular shape
allows the bottom end of the shaft 31 to pass through its inside
and is fixed at the bottom end of the shaft 31. Thrust
20 dynamic-pressure generating grooves 33A and 33B are provided on
surfaces of the flange 33. An outer surface of a sleeve 32 is fixed

on a base 35, and an inner surface 32A of the sleeve 32 surrounds the shaft 31. The flange 33 is then placed in a hollow 32D formed by a bottom surface of the sleeve 32 and an inner surface of the base 35. A thrust plate 34 is fixed on the base 35 and closes the lower side of a space surrounded by the sleeve 32 and the base 35. The upper surface of the thrust plate 34 is then opposed to the lower surface of the flange 33. In this hydrodynamic bearing, in particular, the thrust plate 34 completely cuts off gaps among the flange 33, the sleeve 32, and the base 35 from the outside space.

Radial dynamic-pressure generating grooves are provided on one or both of a side of the shaft 31 and an inner surface of the sleeve 32. Radial dynamic-pressure generating grooves are usually provided on two regions, a first region 32B near the flange 33 and a second region 32C near the upper opening end of the sleeve 32 (see broken lines shown in FIG. 6.) The thrust dynamic-pressure generating grooves 33A and 33B and the radial dynamic-pressure generating grooves 32B and 32C are, for example, herringbone-shaped grooves. Gaps among the shaft 31, the sleeve 32, the thrust plate 34, and the base 35 are filled with oil 42. Magnetic disks 39 are fixed on the outer surface of the hub 36, being concentric with the shaft 31. Generally, several sheets of the magnetic disks 39 are installed. The spacers 40 are installed between inner radii of the magnetic disks 39, and the clamper 41 further presses down the inner radii of the magnetic disks 39 from the top. Thereby, the magnetic disks 39 are fixed on the hub 36. Magnets 38 are installed on the inner surfaces of the hub 36. On the other hand,

stators 37 are installed on the base 35 and opposed to the magnets 38.

The above-described hydrodynamic bearing operates as follows. Rotating magnetic fields occur when the stators 37 are energized.

5 The hub 36 undergoes a torque from the rotating magnetic fields through the magnets 38. Thereby, the shaft 31, the hub 36, and the magnetic disks 39 revolve in a body around the shaft 31. During the revolution, the oil 42 flows along the radial dynamic-pressure generating grooves and is concentrated in each central part of the
10 first region 32B and the second region 32C. As a result, pressure in the radial direction of the shaft 31 is enhanced in those central parts. This pumping effect maintains stable spacing between the shaft 31 and the sleeve 32, and thereby the rotation axis of the magnetic disks 39 does not substantially shift in the radial
15 direction of the shaft 31. Similarly, the oil 42 flows along the thrust dynamic-pressure generating grooves 33A and 33B and is concentrated in each central part of regions where the thrust dynamic-pressure generating grooves 33A and 33B are provided. As a result, pressure in the axial direction of the shaft 31 is enhanced
20 on surfaces of the flange 23. This pumping effect maintains stable spacing between the flange 33 and the sleeve 32 and stable spacing between the flange 33 and the thrust plate 34. Therefore, the rotation axis of the magnetic disks does not substantially tilt from the axial direction of the shaft 31. Thus, the above-described
25 hydrodynamic bearing maintains the high-speed revolution of the

magnetic disks 39 stable with high precision.

In such a conventional hydrodynamic bearing as the above-described one, the above-described pumping effects are fully exerted under the condition with the oil 42 covering the whole of the radial dynamic-pressure generating grooves 32B and 32C and the whole of the thrust dynamic-pressure generating grooves 33A and 33B. However, an abundance of minute air bubbles (microbubbles) intrudes into the oil 42, for example, after a time lapse of use. The microbubbles accumulate particularly in spaces where pressure is low among gaps filled with the oil 42, and then agglomerate into large air bubbles there. FIG. 7 is a cross-sectional view showing positions where the air bubbles tend to appear. The air bubbles 43 tend to accumulate in the intermediate region 32E between the first region 32B and the second region 32C, the perimeter of the flange 33, and their vicinities, as shown in FIG. 7. When those air bubbles are large and many, or when those swell with variations of outside air pressure or temperature rises of the oil 42, the oil 42 is pushed and shifts by the pressure of the air bubbles. Thereby, the oil 42 tends to escape outward from the gap between the top of the shaft 31 and the upper opening of the sleeve 32 (see droplets 42A shown in FIG. 7.) Furthermore, a so-called lack of oil film, that is, a condition that the oil 42 fails to cover the whole of the radial dynamic-pressure generating grooves and the thrust dynamic-pressure generating grooves, occurs when the amount of leakage of the oil 42 is excessive. In that case, the

above-described pumping effects become insufficient, and this increases, for example, the risk of excessively hard contact between the shaft 31 and the sleeve 32 or between the flange 33 and the thrust plate 34 resulting in serious wear of them.

5 SUMMARY OF THE INVENTION

An object of the present invention is to provide a hydrodynamic bearing that prevents in gaps the agglomeration of microbubbles intruding inside a lubricant by allowing them to easily escape out of the gaps, and reliably maintains a lubricant-filled
10 condition of the whole of radial dynamic-pressure generating grooves and thrust dynamic-pressure generating grooves, thereby ensuring high reliability.

A hydrodynamic bearing according to the present invention comprises:

15 (a) a shaft;

(b) a flange being a substantial disc and fixed on one end of the shaft;

(c) a sleeve, when the shaft is inserted into its inside, allowed to revolve around the shaft and placed where a hollow
20 provided on an inner surface of the sleeve is in the vicinity of a surface of the flange;

(d) a thrust plate hermetically sealing a first opening end of the sleeve, thereby being placed close to the flange when the

shaft is inserted inside the sleeve; and

(e) a lubricant with which the whole of radial dynamic-pressure generating grooves provided at least one of a side of the shaft and an inner surface of the sleeve, and the whole of thrust dynamic-pressure generating grooves provided at least one of the surfaces of the flange and the thrust plate opposed to each other, are filled and covered. In this hydrodynamic bearing, in particular, inequalities $A < B$, $A < D$, $C < B$, $C < D$, $B < H$, $D < H$, and $G < H$ all hold, where A is a distance in the axial direction of the shaft between the flange and the thrust plate over the thrust dynamic-pressure generating groove and its vicinity, B is a distance in the radial direction of the shaft between a perimeter of the flange and the above-described hollow of the sleeve, C is a distance in the axial direction of the shaft between the flange and the above-described hollow of the sleeve, D is a distance in the radial direction of the shaft between the shaft and the sleeve around the joint between the shaft and the flange, G is a distance in the radial direction of the shaft between the shaft and the sleeve over the radial dynamic-pressure generating groove and its vicinity, and H is a distance in the radial direction of the shaft between the shaft and the sleeve at a second opening end of the sleeve.

For example, a disk recording/reproducing apparatus is equipped with this hydrodynamic bearing according to the present invention. Here, the disk recording/reproducing apparatus comprises:

(a) a base on which one of the shaft and the sleeve is fixed;

(b) a hub connected to another of the shaft and the sleeve that is not fixed on the base and allowed to revolve around the shaft;

5 (c) a motor installed between the base and the hub, including a magnet and a coil, and for exerting to the hub a torque for a revolution around the shaft;

(d) a magnetic disk concentrically fixed on the hub; and

(e) a head, when the magnetic disk revolves because of the
10 torque, being placed close to a surface of the magnetic disk, recording a signal onto the magnetic disk, and reproducing a signal from the magnetic disk.

In the above-described hydrodynamic bearing according to the present invention, the lubricant flows along the radial
15 dynamic-pressure generating grooves and is concentrated in predetermined regions when the shaft or the sleeve revolves around the shaft. As a result, pressure in the radial direction of the shaft rises in gaps between the shaft and the sleeve. This pumping effect maintains stable spacing between the shaft and the sleeve,
20 and thus, the axis of rotation of the shaft or the sleeve does not substantially shift in the radial direction of the shaft. Similarly, the lubricant flows along the thrust dynamic-pressure generating grooves and is concentrated in predetermined regions. As a result, pressure in the axial direction of the shaft rises
25 on surfaces of the flange. This pumping effect maintains stable

spacing between the flange and the hollow of the sleeve and stable spacing between the flange and the thrust plate. Therefore, the axis of rotation of the shaft or the sleeve does not substantially tilt from the axial direction of the shaft. Thus, the

5 above-described hydrodynamic bearing according to the present invention maintains high-speed revolutions of the shaft or the sleeve stable with high precision.

In the above-described hydrodynamic bearing according to the present invention, gaps among the sleeve, the shaft, the flange,
10 and the thrust plate are set as described above. More specifically, the gaps over the thrust dynamic-pressure generating grooves and their vicinities are narrower than the surrounding gaps. Furthermore, the surrounding gaps are narrower than the gaps in the second opening end of the sleeve and its vicinity. In addition,
15 the gaps over the radial dynamic-pressure generating grooves and their vicinities are narrower than the gaps in the second opening end of the sleeve and its vicinity. In that case, the sealing force of lubricant is the strongest over the thrust dynamic-pressure generating grooves and their vicinities, next stronger in the gaps
20 surroundings the flange, and the weakest in the second opening end of the sleeve and its vicinity. Furthermore, the sealing force over the radial dynamic-pressure generating grooves and their vicinities is stronger than the sealing force in the second opening end of the sleeve and its vicinity. Such a gradient of sealing force keeps
25 microbubbles in the lubricant away from the vicinities of the thrust

dynamic-pressure generating grooves and the radial
dynamic-pressure generating grooves, and, in addition, pushes them
back into the second opening end of the sleeve. The microbubbles,
in particular, hardly reach in the vicinity of the perimeter of
5 the flange. Thus, occurrences of the air bubbles due to the
agglomeration of the microbubbles are prevented, and leakage of
lubricant due to the occurrence and swelling of the air bubbles
are avoided. Accordingly, the lubricant keeps covering the whole
of the radial dynamic-pressure generating grooves and the thrust
10 dynamic-pressure generating grooves with stability, that is, no
so-called lack of oil film occurs. In other words, the
above-described pumping effects are maintained with stability, and
thus, spacing between the shaft and the sleeve is maintained with
stability. Therefore, the above-described hydrodynamic bearing
15 according to the present invention has high reliability.

In the above-described hydrodynamic bearing according to the
present invention, the radial dynamic-pressure generating grooves
may be provided in two regions, a first region near the flange and
a second region near the second opening end of the sleeve. In that
20 case, it is preferable that inequalities $E < D$, $E < F$, $G < D$, $G < F$, and
 $F < H$ all hold, where E is a distance in the radial direction of the
shaft between the shaft and the sleeve in the first region, F is
a distance in the radial direction of the shaft between the shaft
and the sleeve in an intermediate region between the first region
25 and the second region, and G is a distance in the radial direction

of the shaft between the shaft and the sleeve in the second region. Thereby, the gaps in the first and second regions and their vicinities, that is, the gaps over the radial dynamic-pressure generating grooves and their vicinities, are narrower than the surrounding gaps. Furthermore, the surrounding gaps are narrower, than the gaps in the second opening end of the sleeve and its vicinity. In that case, the sealing force of lubricant is the strongest over the radial dynamic-pressure generating grooves and their vicinities, next stronger in the gaps in an intermediate region between the second region and the flange and its vicinity, and the gaps in the intermediate region between the first region and the second region and its vicinity, and the weakest in the second opening end of the sleeve and its vicinity. Such a gradient of sealing force keeps microbubbles in the lubricant away from the vicinities of the radial dynamic-pressure generating grooves, and, in addition, pushes them back into the second opening end of the sleeve. The microbubbles, in particular, hardly accumulate in the intermediate region between the first region and the second region. Thus, occurrences of the air bubbles due to the agglomeration of the microbubbles are prevented, and leakage of lubricant due to the occurrence and swelling of the air bubbles are avoided. Accordingly, the lubricant keeps covering the whole of the radial dynamic-pressure generating grooves with stability, that is, no so-called lack of oil film occurs. In other words, the above-described, radial pumping effect is maintained with stability, and thus, spacing between the shaft and the sleeve is maintained with stability.

Therefore, the above-described hydrodynamic bearing according to the present invention has still higher reliability.

In the above-described hydrodynamic bearing according to the present invention, preferably, the lubricant is composed of one
5 of oil and grease, and shows a kinematic viscosity of at least $4 \times 10^{-6} \text{ m}^2/\text{s}$ at 40 degrees centigrade. Such a lubricant remarkably reduces a rate of the intrusion of air bubble. For example, ester oil or ester oil of neopentyl glycol is suitable for the above-described lubricant. The utilization of such a lubricant
10 further effectively prevents leakage of lubricant due to the occurrence and swelling of air bubbles. Accordingly, the above-described hydrodynamic bearing according to the present invention has still higher reliability.

The above-described hydrodynamic bearing according to the
15 present invention has high reliability as described above. When a disk recording/reproducing apparatus is equipped with the hydrodynamic bearing, the revolution of magnetic disks can further become faster and be further stabilized with higher precision in the disk recording/reproducing apparatus. As a result, increases
20 in capacity and speedups of data transfers can be easily enhanced. In addition, the disk recording/reproducing apparatus can maintain high reliability for a long time.

While the novel features of the invention are set forth particularly in the appended claims, the invention, both as to

organization and content, will be better understood and appreciated, along with other objects and features thereof, from the following detailed description taken in conjunction with the drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

5 FIG. 1 is a cross-sectional view of a hydrodynamic bearing according to an embodiment of the present invention;

FIG. 2 is a cross-sectional view showing details of the hydrodynamic bearing according to the embodiment of the present invention;

10 FIG. 3 is a cross-sectional view showing an example of variations of the hydrodynamic bearing according to the embodiment of the present invention;

FIG. 4 is a graph showing a relation between gap sizes and sealing forces of lubricant for the hydrodynamic bearing according
15 to the embodiment of the present invention;

FIG. 5 is a cross-sectional view of a disk recording/reproducing apparatus according to the embodiment of the present invention;

FIG. 6 is a cross-sectional view of an example of conventional
20 hydrodynamic bearings.

FIG. 7 is a cross-sectional view showing positions where air bubbles tend to appear, for the conventional hydrodynamic bearing

shown in FIG. 6.

It will be recognized that some or all of the Figures are schematic representations for purposes of illustration and do not necessarily depict the actual relative sizes or locations of the elements shown.

DETAILED DESCRIPTION OF THE INVENTION

The following describes the best embodiments of the present invention, with referring to the figures.

FIG. 5 is a cross-sectional view of a disk recording/reproducing apparatus according to an embodiment of the present invention. This disk recording/reproducing apparatus comprises a base 6, a hydrodynamic bearing, a hub 7, stators 8, magnets 9, magnetic disks 10, a clamper 11, spacers 12, a cover 14, swing arms 15, and a support 16. The hydrodynamic bearing comprises a sleeve 1, a shaft 2, a flange 3, and a thrust plate 4. The base 6 and the cover 14 are fit to each other, thereby forming a box-shaped cabinet. Then, the base 6 and the cover 14 enclose the inside of the cabinet, thereby protecting it against intrusion by foreign substances such as dust from the outside. The sleeve 1 is inserted into a hole in the base 6 and is fixed there. The thrust plate 4 hermetically seals the lower opening end of the sleeve 1. Here, the thrust plate 4 is fixed at the lower opening end of

the sleeve 1 by, for example, laser welding, precision swaging, or bonding. Alternatively, the thrust plate 4 may be fixed on the base 6. The shaft 2 is inserted into the sleeve 1 and allowed to revolve around itself. The flange 3 is fixed on the bottom end of the shaft 2, and then its lower surface is placed close to the upper surface of the thrust plate 4. The top end of the shaft 2 is fixed to the hub 7 with a screw 13. Thus, the hub 7 surrounding the sleeve 1 revolves around the shaft 2. Alternatively, the shaft 2 may be fixed on the base 6 and the sleeve 1 may be fixed to the hub 7. In that case, the hub 7 revolves around the shaft 2 together with the sleeve 1. The magnetic disks 10 are fixed on outer surfaces of the hub 7, being concentric with the shaft 2. For example, several sheets of the magnetic disks 10 are installed. Here, the number of the magnetic disk 10 may be one. The spacers 12 are installed between inner radii of the magnetic disks 10, and, in addition, the clamper 11 presses down the inner radii of the magnetic disks 10 from the top. Thereby, the magnetic disks 10 are fixed on the hub 7. The stators 8 are fixed on the base 6 around the sleeve 1. On the other hand, the magnets 9 are installed on inner surfaces of the hub 7 and opposed to the stators 8. The bottom end of the support 16 is fixed on the base 6. The swing arms 15 comprise the heads 18 at their tips, and are connected at their rear ends to the support 16, being allowed to swing. One of the swing arms 15 is provided for one side each of the magnetic disks 10.

FIG. 1 is a cross-sectional view of the above-described

hydrodynamic bearing. Radial dynamic-pressure generating grooves are provided, for example, in two separated regions on the inner surface of the sleeve 1 (see broken lines shown in FIG. 1.) Of those two regions, let a first region 1A be one region in the flange 3 side and a second region 1B be another region in the base 1 side. Radial dynamic-pressure generating grooves may be provided on the side of the shaft 2 instead of or in addition to the inner surface of the sleeve 4. Radial dynamic-pressure generating grooves are, for example, herringbone-shaped grooves. Alternatively, radial dynamic-pressure generating grooves may be shaped into spirals. A hollow 1C is provided at the lower opening end of the inner surface of the sleeve 4. The flange 3 is placed inside the hollow 1C. Thrust dynamic-pressure generating grooves 3A and 3B are provided on upper and lower surfaces of the flange 3, respectively. Alternatively, thrust dynamic-pressure generating grooves may be provided only on one side of the flange 3. Thrust dynamic-pressure generating grooves may be provided on one or both of a surface of the above-described hollow 1C of the sleeve 4 and the upper surface of the thrust plate 4, instead of or in addition to the surface of the flange 3. Thrust dynamic-pressure generating grooves are, for example, herringbone-shaped grooves. Alternatively, thrust dynamic-pressure generating grooves may be shaped into spirals. A lubricant 5 is preferably oil, or alternatively, may be grease. With the lubricant 5, gaps between the sleeve 1 (or the thrust plate 4) and the shaft 2 (or the flange 3) are filled.

When the above-described disk recording/reproducing apparatus performs recording/reproducing of data for the magnetic disks 10, the above-described hydrodynamic bearing operates as follows (see FIGs. 1 and 5.) Rotating magnetic fields occur when the stators 8 are energized. The hub 7 undergoes a torque from the rotating magnetic fields through the magnets 9. Thereby, the shaft 2, the hub 7, and the magnetic disks 10 in a body revolve around the shaft 2. During the revolution, the lubricant 5 flows along the radial dynamic-pressure generating grooves in the first region 1A and the second region 1B and their vicinities, and is concentrated in the central parts of the respective regions. As a result, pressure in the radial direction of the shaft 2 rises in those central parts. This pumping effect maintains stable spacing between the sleeve 1 and the shaft 2, and thereby, the axis of revolution of the magnetic disks 10 does not substantially shift in the radial direction of the shaft 2. Similarly, the lubricant 5 flows along the thrust dynamic-pressure generating grooves 3A and 3B on the surfaces of the flange 3, and is concentrated on the middle parts of the respective surfaces of the flange 3. As a result, pressure in the axial direction of the shaft 2 rises on the surfaces of the flange 3. This pumping effect maintains stable spacing between the hollow 1C at the lower opening end of the sleeve 1 and the flange 3, and stable spacing between the flange 3 and the thrust plate 4. Therefore, the axis of revolution of the magnetic disks 10 does not substantially tilt from the axial direction of the shaft 2. Thus, the above-described hydrodynamic bearing maintains the

high-speed revolution of the magnetic disks 10 stable with high precision.

At the high-speed revolution of the magnetic disks 10, the swing arms 15 swing around the support 16, and move the heads 18 to destinations over the magnetic disks 10. Here, the head 18 floats at a minute distance from the surface of the magnetic disk 10 because of the high-speed revolution of the magnetic disk 10. At the destinations over the magnetic disks 10, the heads 18 write data onto the magnetic disks 10, or read data from the magnetic disks 10. Here, the above-described hydrodynamic bearing maintains the high-speed revolution of the magnetic disks 10 stable with high precision, and therefore the reading and writing of data by the heads 18 have high reliability.

In the above-described hydrodynamic bearing according to the embodiment of the present invention, in particular, the gaps among the sleeve 1, the shaft 2, the flange 3, and the thrust plate 4 vary in size from place to place as follows. FIG. 2 is a cross-sectional view showing details of the above-described hydrodynamic bearing. A plurality of hollows is provided on the inner surface of the sleeve 1. Those hollows are, in ascending order of vertical position, the hollow 1C at the lower opening end, a small hollow 1D immediately above it, an intermediate region 1E between the first region 1A and the second region 1B, and a hollow 1F at the upper opening end. Axial and radial directions hereafter refer to the axial and radial directions of the shaft 2, respectively.

Let A be an axial distance in the gap A between the thrust plate 4 and the thrust dynamic-pressure generating grooves 3A on the lower surface of the flange 3, B be a radial distance in the gap B between the perimeter of the flange 3 and the hollow 1C at the lower opening end of the sleeve 1, C be an axial distance in the gap C between the thrust dynamic-pressure generating grooves 3B on the upper surface of the flange 3 and the hollow 1C at the lower opening end of the sleeve 1, D be a radial distance in the gap D between the small hollow 1D of the sleeve 1 and the shaft 2, E be a radial distance in the gap E between the first region 1A of the sleeve 1 and the shaft 2, F be a radial distance in the gap F between the intermediate region 1E of the sleeve 1 and the shaft 2, G be a radial distance in the gap G between the second region 1B of the sleeve 1 and the shaft 2, and H be a radial distance in the gap H between the hollow 1F at the upper opening end of the sleeve 1 and the shaft 2 (here, the gaps and the distances are represented by the same reference symbols in order to clarify the correspondences between them.)

Then, inequalities $A < B$, $A < D$, $C < B$, $C < D$; $B < H$, $D < H$; $E < D$, $E < F$, $G < D$, and $G < F < H$ all hold. In other words, the gaps A and C in the thrust dynamic-pressure generating grooves 3A and 3B and their vicinities are narrower than the surrounding gaps B and D ($A < B$, $A < D$, $C < B$, $C < D$), and the surrounding gaps B and D are narrower than the gap H at the upper opening end of the sleeve 1 and its vicinity ($B < H$, $D < H$.)

In addition, the gaps E and G in the radial dynamic-pressure generating grooves and their vicinities are narrower than the surrounding gaps D and F ($E < D$, $E < F$, $G < D$, $G < F$), and the surrounding

gaps D and F are narrower than the gap H at the upper opening end of the sleeve 1 and its vicinity ($D < H$, $F < H$.)

Generally, the narrower gaps, the stronger the sealing force of the lubricant 5 with which the gaps are filled. FIG. 4 is a graph showing a relation between gap sizes and sealing forces of the lubricant 5 for the hydrodynamic bearing according to the embodiment of the present invention. In FIG. 4, the horizontal and vertical axes show gap sizes in micrometers (μm) and sealing forces in Pascals (Pa), respectively. FIG. 4, in particular, shows an example of correspondences between gap sizes and sealing forces of the lubricant 5 for the respective gaps A, B, C, ..., and H shown in FIG. 2. As shown in FIG. 4, the sealing force of the lubricant 5 is the strongest in the gaps A and C over the thrust dynamic-pressure generating grooves and their vicinities and the gaps E and G over the radial dynamic-pressure generating grooves and their vicinities, next stronger in their surrounding gaps B, D, and F, and the weakest in the gap H at the upper opening end of the sleeve 1 and its vicinity. Such a gradient of sealing force keeps microbubbles in the lubricant 5 away from the vicinities A and C of the thrust dynamic-pressure generating grooves and the vicinities E and G of the radial dynamic-pressure generating grooves, and further pushes them back into the upper opening end of the sleeve 1. The microbubbles, in particular, hardly accumulate in the gap in the intermediate region 1E of the sleeve 1 and its vicinity, and, in addition, hardly reach the gap B around the perimeter of

the flange 3 and its vicinity. Thus, occurrences of air bubbles due to the agglomeration of the microbubbles are prevented, and leakage of the lubricant 5 due to the occurrence and swelling of the air bubbles are avoided. Accordingly, the lubricant 5 keeps
5 covering the whole of the radial dynamic-pressure generating grooves and the thrust dynamic-pressure generating grooves with stability, that is, no so-called lack of oil film occurs. In other words, the above-described pumping effects are maintained with stability, and thus, spacing between the sleeve 1 and the shaft
10 2 is maintained with stability. Therefore, the above-described hydrodynamic bearing according to the embodiment of the present invention has particularly high reliability.

FIG. 4 is only one example out of many, showing the correspondences between the sizes of the gaps A-H and the sealing
15 forces of the lubricant 5 shown in FIG. 2. In order to cause the sealing forces of the lubricant 5 to prevent the microbubbles from intruding into the lubricant 5 as described above, the gaps A-H may be set as follows. Radial distances may be set in the 1-10 μm range in the gap E in the first region 1A and its vicinity and
20 the gap G in the second region 1B and its vicinity. Axial distances may be set in the 10-60 μm range in the gaps A and C in the thrust dynamic-pressure generating grooves 3A and 3B and their vicinities. Radial distances may be set in the 20-100 μm range in the gaps D and F in the adjacent regions of the first region 1A. A radial
25 distance may be set in the 50-300 μm range in the gap B between the

hollow 1C at the lower opening end of the sleeve 1 and the perimeter of the flange 3. A radial distance may be set in the 50-800 μm range in the gap H between the shaft 2 and the hollow 1F at the upper opening end of the sleeve 1.

5 In the above-described hydrodynamic bearing according to the embodiment of the present invention, preferably, the lubricant 5 shows a kinematic viscosity of at least $4 \times 10^{-6} \text{ m}^2/\text{s}$ at 40 degrees centigrade. When the kinematic viscosity of the lubricant 5 satisfies the condition, a rate of the intrusion of air bubble is
10 remarkably reduced. This fact is revealed by the construction of the above-described hydrodynamic bearing from transparent members and the observation of the intrusion of the microbubbles into the lubricant 5 during the operation. Accordingly, ester oil or ester
15 oil of neopentyl glycol, for example, is suitable for the lubricant 5. The utilization of such a lubricant 5 further effectively prevents leakage of the lubricant 5 due to the occurrence and swelling of air bubbles. Accordingly, the above-described hydrodynamic bearing according to the present invention has still higher reliability.

20 In the above-described hydrodynamic bearing according to the embodiment of the present invention, a similar plurality of hollows may be provided on the side of the shaft 2, instead of or in addition to the inner surface of the sleeve 1. Furthermore, shapes other than the above-described plurality of the hollows 1C-1F may be added
25 on the inner surface of the sleeve 1, the side of the shaft 2, or

the surfaces of the flange 3. FIG. 3 is a cross-sectional view showing details of a variation of the hydrodynamic bearing according to the embodiment of the present invention. In FIG. 3, components similar to components shown in FIG. 2 are marked with the same reference symbols as the reference symbols shown in FIG. 2. A hollow 3C may be provided on the inner radius of the lower surface of the flange 3, as shown in FIG. 3. In that case, the gap under the flange 3 at the inner radii of the flange 3 and the vicinity J is broader than the gap over the thrust dynamic-pressure generating grooves 3A and their vicinity A. Accordingly, the sealing force of the lubricant 5 at the inner radii of the flange 3 and the vicinity J is weaker than the sealing force over the thrust dynamic-pressure generating grooves 3A and their vicinity A (see FIG. 4.) Therefore, the lubricant 7 in the gap under the flange 3 is concentrated particularly over the thrust dynamic-pressure generating grooves 3A and their vicinity A, thus keeping reliably covering the whole of the thrust dynamic-pressure generating grooves 3A. In addition, let H be a distance in the radial direction of the shaft 2 in the gap H between the hollow 1F at the upper opening end of the sleeve 1 and the shaft 2, and J be a distance in the axial direction of the shaft 2 in the gap J at the inner radii of the flange 3 and the vicinity, then an inequality $J < H$ holds. For example, the above-described distance J in the gap J at the inner radii of the flange 3 and the vicinity may be set in the 50-300 μm range. Then, the sealing force of the lubricant 5 at the inner radii of the flange 3 and the vicinity J is stronger than the sealing force in the hollow

1F at the upper opening end of the sleeve 1 and its vicinity H (see FIG. 4.) As a result, the microbubbles hardly accumulate into the inner radii of the flange 3 and the vicinity J.

A small protrusion 1G may be further provided to be adjacent to the upper side of the hollow 1F of the upper opening end of the sleeve 1, as shown in FIG. 3. The small protrusion 1G narrows the area of the upper opening of the sleeve 1, thereby protecting the gaps between the sleeve 1 and the shaft 2 against intrusion by dust and air. Here, the existence of the small protrusion 1G of the sleeve 1 does not impair the above-described effect due to the gap H between the hollow 1F at the upper opening end of the sleeve 1 and the shaft 2 larger than the other gaps A-G, that is, the elimination effect of microbubbles due to the gradient of the sealing force.

The hydrodynamic bearing according to the present invention maintains the high-speed revolution of the sleeve stable with high precision and prevents leakage of lubricant due to the agglomeration of microbubbles, as described above, thereby having high reliability. Disk recording/reproducing apparatuses equipped with these hydrodynamic bearings can easily realize further increases in capacity and further speedups of data transfer, and maintain high reliability for a long time. Accordingly, the installation of the hydrodynamic bearings on disk recording/reproducing apparatuses has very high utility in industry.

The above-described disclosure of the invention in terms of the presently preferred embodiments is not to be interpreted as intended for limiting. Various alterations and modifications will no doubt become apparent to those skilled in the art to which the invention pertains, after having read the disclosure. As a corollary to that, such alterations and modifications apparently fall within the true spirit and scope of the invention. Furthermore, it is to be understood that the appended claims be intended as covering the alterations and modifications.